The surface-atmosphere interactionS

The surface-atmosphere interaction^S

- **1. Introduction, process involved**
- **2. Radiation over sub-surfaces**
- **3. Turbulent transport**
- **4. Surface energy budget and heat diffusion into the soil**
- **5. Fully coupled surface – atmosphere system**
- **6. Some illustration of the coupling**
- **7. Call tree in LMDZ**
- **8. Take home messages**

Radiation at the surface

depends on mean surface properties (albedo, emissivity)

Turbulent diffusion

depends on local sub-grid properties (roughness)

Turbulent diffusion depends on local sub-grid properties (roughness)

Radiation at the surface depends on mean surface properties (albedo, emissivity)

In LMDZ : 4 sub-surfaces : land, land-ice, ocean, sea-ice

Each grid cell is divided into several sub-areas or ``sub-surfaces'' of fractions

$$
\sum_i \omega_i = 1
$$

One atmospheric column **covers all** the sub-surface

The grid average net flux SW_{net} has been computed previously by the radiative code

We need to (1) conserve energy and (2) take into account the value α_i of the local albedo of the sub-surface i

$$
SW_{dn} = \frac{SW_{net}}{(1-\alpha)} \qquad \alpha = \sum_{i} \omega_i \alpha_i
$$

$$
SW_{net}^i = (1-\alpha_i)SW_{dn} = \frac{(1-\alpha_i)}{(1-\alpha)}SW_{net}
$$

$$
\sum_i \omega_i \mathbf{SW}_{net}^i = \mathbf{SW}_{net}
$$

The grid average net flux SW_{net} has been computed previously by the radiative code

We need to (1) conserve energy and (2) take into account the value of the surface temperature (emissivity) of the sub-surface i

$$
LW_{net}^{i}(T_{s}^{i}) = \epsilon_{i}(LW_{dn} - \sigma(T_{s}^{i})^{4})
$$
\n
$$
T_{s}^{i4} \approx T_{s}^{4} + 4T_{s}^{3}(T - T_{s}^{i})
$$
\n
$$
LW_{net}(T_{s}) = \epsilon(LW_{dn} - \sigma(T_{s}^{i})^{4}) - 4\sigma T_{s}^{3} \sum \omega_{i}\epsilon_{i}(T_{s}^{i} - T_{s}) \qquad \epsilon = \sum_{i} \omega_{i}\epsilon_{i}
$$
\n
$$
4\sigma T_{s}^{3} \sum \omega_{i}\epsilon_{i}(T_{s}^{i} - T_{s}) = 0 \qquad \text{Energy conservation}
$$
\n
$$
T_{s} = \frac{\sum \omega_{i}\epsilon_{i}T_{s}^{i}}{\epsilon}
$$

Due to radiative code limitation, in LMDZ, we always must have $\varepsilon_i = 1$

Each grid cell is divided into several sub-areas or ``sub-surfaces'' of fractions

$$
\sum_i \omega_i = 1
$$

In the timestep :one PBL over **each** subsurface

Vertical turbulent diffusion for moisture, heat , momentum

Time evolution of a variable X due to turbulent transport as the divergence of the turbulent flux:

 $\begin{cases} \frac{\partial X}{\partial t} = -\frac{1}{\rho} \frac{\partial \Phi}{\partial z} \\ \Phi = -W^T X' = -\rho k_z \frac{\partial X}{\partial z} \end{cases}$ with

 k_z : the vertical turbulent diffusion coefficient for X

in the atmosphere

$$
\frac{\partial X}{\partial t} = -\frac{1}{\rho} \frac{\partial [-\rho k_z \frac{\partial X}{\partial z}]}{\partial z}
$$

Vertical turbulent diffusion for moisture, heat , momentum

Time evolution of a variable X due to turbulent transport as the divergence of the turbulent flux:

$$
\begin{cases} \frac{\partial X}{\partial t} = -\frac{1}{\rho} \frac{\partial \Phi}{\partial z} \\ \Phi = -\mathbf{w}^T \mathbf{X}' = -\rho \mathbf{k}_z \frac{\partial X}{\partial z} \quad \text{with} \end{cases}
$$

 k_z : the vertical turbulent diffusion coefficient for X

in the atmosphere

$$
\frac{\partial X}{\partial t} = -\frac{1}{\rho} \frac{\partial [-\rho k_z \frac{\partial X}{\partial z}]}{\partial z}
$$

 $,q^* =$

 $\overline{w'q'}$

 u_*

 $u_*^2 = \frac{\tau}{a}$ $\frac{\tau}{\rho} = -\overline{u'w'}$, $\theta^* = \frac{w'\theta'}{u_*}$ Surface layer, constant flux:

MOST, flux-gradient (Neutral)

 $\frac{\partial u}{\partial z}\frac{\kappa z}{u_*}=1$

 $\frac{\partial \Theta}{\partial z}\frac{\kappa z}{\Theta_z}=1$

 u_*

 $=\frac{H}{\sqrt{2}}$

 $\rho c_p u_*$

 $\frac{\partial X}{\partial t} = -\frac{1}{\rho} \frac{\partial [-\rho k_z \frac{\partial X}{\partial z}]}{\partial z}$

 z_{0u}

Vertical turbulent diffusion for moisture, heat , momentum

Time evolution of a variable X due to turbulent transport as the divergence of the turbulent flux:

$$
\begin{cases} \frac{\partial X}{\partial t} = -\frac{1}{\rho} \frac{\partial \Phi}{\partial z} \\ \Phi = -\mathbf{w}^T \mathbf{X}' = -\rho \mathbf{k}_z \frac{\partial X}{\partial z} \quad \text{with} \end{cases}
$$

 k_z : the vertical turbulent diffusion coefficient for X

Surface layer :constant flux:

MOST, flux-gradient

(Neutral)

x:
$$
u_*^2 = \frac{\tau}{\rho} = -\overline{u'w'}, \ \theta^* = \frac{\overline{w'\theta'}}{u_*} = \frac{H}{\rho c_p u_*}, \ \ q^* = \frac{\overline{w'}q'}{u_*}
$$

\n $\frac{\partial u}{\partial z} \frac{\kappa z}{u_*} = 1$
\n $\frac{\partial u}{\partial z} \frac{\kappa z}{u_*} = 1$
\n $\int_{u_0}^{u_1} \partial u = \int_{z_0}^{z_1} \frac{u_*}{\kappa z} dz$
\n $\int_{\theta_1}^{u_1} \partial u = \int_{z_0}^{z_1} \frac{u_*}{\kappa z} dz$
\n $\int_{\theta_s}^{\theta_1} \partial \Theta = \int_{z_0}^{z_1} \frac{\kappa \Theta_*}{z} dz$
\n $\int_{\theta_1}^{z_1} \frac{\kappa \Theta_*}{z_0} dz$
\n $\int_{\theta_2}^{z_1} \frac{u_*}{\theta} du = \int_{\theta_1}^{z_1} \frac{u_*}{\theta} du$
\n $\int_{\theta_2}^{z_1} \frac{u_*}{\theta} du = \int_{z_0}^{z_1} \frac{u_*}{\theta} du$
\n $\int_{\theta_3}^{z_1} \frac{u_*}{\theta} du = \int_{z_0}^{z_1} \frac{u_*}{\theta} du$

Vertical turbulent diffusion for moisture, heat , momentum

Time evolution of a variable X due to turbulent transport as the divergence of the turbulent flux:

$$
\begin{cases} \frac{\partial X}{\partial t} = -\frac{1}{\rho} \frac{\partial \Phi}{\partial z} \\ \Phi = -\mathbf{w}^T \mathbf{X}' = -\rho \mathbf{k}_z \frac{\partial X}{\partial z} \end{cases}
$$
 with

$$
\frac{\partial X}{\partial t} = -\frac{1}{\rho} \frac{\partial [-\rho \kappa_z \frac{\partial}{\partial z}]}{\partial z}
$$

 Ω

 $\overline{1}$ of $\overline{1}$ ∂X

 k_z : the vertical turbulent diffusion coefficient for X

Surface layer :constant flux:

MOST, flux-gradient

(Neutral)

$$
u_{*}^{2} = \frac{\tau}{\rho} = -\overline{u'w'}, \ \theta^{*} = \frac{\overline{w'\theta'}}{u_{*}} = \frac{H}{\rho c_{p}u_{*}}, \ \ q^{*} = \frac{\overline{w'q'}}{u_{*}}
$$
\n
$$
\frac{\partial u}{\partial z}\frac{kZ}{u_{*}} = 1 \qquad \frac{\partial \Theta}{\partial z}\frac{kZ}{\Theta_{*}} = 1
$$
\n
$$
\int_{u_{0}}^{u_{1}} \partial u = \int_{z_{0}}^{z_{1}} \frac{u_{*}}{\kappa z} dz \qquad \int_{\Theta_{s}}^{\Theta_{1}} \partial \Theta = \int_{z_{0}}^{z_{1}} \frac{\kappa \Theta_{*}}{z} dz
$$
\n
$$
u_{1} - u_{0} = \frac{u_{*}}{\kappa} \ln \frac{z_{1}}{z_{0}} \qquad \Theta_{*} = (\Theta_{1} - \Theta_{s}) \frac{\kappa}{\ln \frac{z_{1}}{z_{0}}}
$$
\n
$$
H = \rho C_{\rho} \kappa^{2} \frac{u_{1}}{\ln \frac{z_{1}}{z_{0}} \ln \frac{z_{1}}{z_{0}} F_{stab(R_{i}, z_{0})} (\Theta_{1} - \Theta_{s})
$$

Turbulent transport: time and space discretization

Numerical world

Tri-diagonal system with implicit boundary condition that can be solved for the vector X= Enthalpy, specific humidity, wind

 $\delta P = (P_{1-1}-P_1) = \rho g \delta z = m_1 g$

X= wind, enthalpie, specific humidity, tracers

Once F_1^x (flux of water mass, heat between the surface and the atmosphere) is known (boundary limit) , the X_i can be computed from the first layer to the top of the PBL

Sensible heat flux **Latent heat flux** $H=C_p\Theta=C_pT(\frac{P}{P_o})^{\kappa}$ $\left\{ \begin{array}{l} F_{\mathbf{s}}^{H,t+\delta t}=\rho |\vec{\mathsf{v}}| C_d (H_{\mathbf{1}}^{t+\delta t}-H_{\mathbf{s}}^{t+\delta t})\[2mm] \ H_{\mathbf{1}}^{t+\delta t}=A_{\mathbf{1}}^{H,t}+B_{\mathbf{1}}^{H,t}F_{\mathbf{s}}^{H,t+\delta t}\delta t \end{array} \right.$

$$
\left\{\begin{aligned} \mathcal{L}_{s}^{q,t+\delta t} &= \rho |\vec{v}| \beta C_{d}(q_{1}^{t+\delta t} - q_{sat}(T_{s}^{t+\delta t})) \\ q_{1}^{t+\delta t} &= A_{1}^{q,t} + B_{1}^{q,t} L_{s}^{q,t+\delta t} \delta t \\ q_{sat}(T_{s}^{t+\delta t}) &= q_{sat}(T_{s}) + \frac{\partial q_{sat}}{\partial T}|_{T_{s}^{t}}(T_{s}^{t+\delta t} - T_{s}^{t}) \end{aligned}\right.
$$

$$
F_s^{H,t+\delta t} = \frac{A_1^{H,t}}{\frac{1}{\rho |\vec{v}| C_d} - B_1^{H,t} \delta t} - \frac{\rho |\vec{v}| C_d}{\frac{1}{\rho |\vec{v}| C_d} - B_1^{H,t} \delta t} H_s^{t+\delta t}
$$

$$
\mathcal{F}_{s}^{H,t+\delta t}= \textit{M}_{\textit{H}}^{t}+\textit{N}_{\textit{H}}^{t} \textit{T}_{s}^{t+\delta t}
$$

$$
C_d = \kappa^2 / (\ln(\frac{z}{zom}) * \ln(\frac{z}{zom})) * Fstab
$$

$$
\mathcal{L}^{q,t+\delta t}_{s}=\mathcal{M}^{t}_{q}+\mathcal{N}^{t}_{q}\mathcal{T}^{t+\delta t}_{s}
$$

 C_d^{χ} drag coefficient (Monin Obukhov, constant flux in the surface layer)

depends on

- roughness lenghts (gustiness, vegetation)
- Richardson number (boundary layer stability)
- Formulation depends on the sub-surface type

Surface energy budget, continuity , heat conduction

Heat conduction

$$
\begin{cases} \frac{\partial T}{\partial t} = -\frac{1}{c_v} \frac{\partial G}{\partial z} \\ G = -\lambda \frac{\partial T}{\partial z} \end{cases}
$$

• Discretization of (1) in space and time

(1)

- $T_{k+1/2}^{t+\delta t} = \alpha_k^t T_{k-1/2}^{t+\delta t} + \beta_k^t$
- (1) for the first interface $G_0 = f(\lambda_i, T_{i+1/2}^{t+\delta t}, \delta z_i, \delta z_{i+1/2})$

Surface energy budget

 LW_{net} + SW_{net} + F_{sens} + F_{lat} = G₀

Surface energy budget, continuity , heat conduction

(1) **Heat conduction**

$$
\begin{cases} \frac{\partial T}{\partial t} = -\frac{1}{c_v} \frac{\partial G}{\partial z} \\ G = -\lambda \frac{\partial T}{\partial z} \end{cases}
$$

- Discretization of (1) in space and time
- $T_{k+1/2}^{t+\delta t} = \alpha_k^t T_{k-1/2}^{t+\delta t} + \beta_k^t$
- \quad (1) for the first interface $\ G_{0}=f(\lambda_{i},\ T^{\iota+\sigma\iota}_{i+1/2},\delta z_{i},\delta z_{i+1/2})$, $\alpha_{\rm k}^{\rm t}\ \beta_{\rm k}^{\rm t}$

Surface energy budget

$$
LW_{\text{net}} + SW_{\text{net}} + F_{\text{sens}} + F_{\text{lat}} + G_0 = 0
$$

$$
C_{p_{1/2}}^{t} \frac{T_{1/2}^{t+\delta t} - T_{1/2}^{t}}{\delta t} = \frac{1}{z_1 - z_0} \left[\lambda_1 \frac{T_{3/2}^{t+\delta t} - T_{1/2}^{t+\delta t}}{z_{3/2} - z_{1/2}} \right] + \sum F^{\downarrow} (T_S^{t+\delta t}) + Rad - \varepsilon \sigma (T_S^{t+\delta t})^4
$$

$$
F_S^{H, t+\delta t} = M_H^t + N_H^t T_S^{t+\delta t} \qquad L_S^{q, t+\delta t} = M_q^t + N_q^t T_S^{t+\delta t}
$$

Surface energy budget, continuity , heat conduction

Heat conduction

$$
\begin{cases} \frac{\partial T}{\partial t} = -\frac{1}{c_v} \frac{\partial G}{\partial z} \\ G = -\lambda \frac{\partial T}{\partial z} \end{cases}
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- Discretization of (1) in space and time
- $T_{k+1/2}^{t+\delta t} = \alpha_k^t T_{k-1/2}^{t+\delta t} + \beta_k^t$
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Surface energy budget

$$
LW_{\text{net}} + SW_{\text{net}} + F_{\text{sens}} + F_{\text{sens}} + F_{\text{lat}} = G_0
$$

$$
C_{p_{1/2}}^{t} \frac{T_{1/2}^{t+\delta t} - T_{1/2}^{t}}{\delta t} = \frac{1}{z_1 - z_0} \left[\lambda_1 \frac{T_{3/2}^{t+\delta t} - T_{1/2}^{t+\delta t}}{z_{3/2} - z_{1/2}} \right] + \sum F^{\downarrow} (T_S^{t+\delta t}) + Rad - \varepsilon \sigma (T_S^{t+\delta t})^4
$$

$$
F_S^{H, t+\delta t} = M_H^t + N_H^t T_S^{t+\delta t} \qquad L_S^{q, t+\delta t} = M_q^t + N_q^t T_S^{t+\delta t}
$$

Temperature continuity : T^s extrapolated from soil temperature

$$
C^{*\frac{T_S^{t+\delta t}-T_S^t}{\delta t}} = G^{t+\delta t}_* + Rad + \sum F^{\downarrow}(T_S^{t+\delta t}) - 4\epsilon\sigma(T_S^t)^3(T_S^{t+\delta t} - T_S^t)
$$

One diffusion equation from the top of the PBL to the bottom of the soil

Some examples : 1D south Great Plaines

ORCHIDEE forcé

ORCHIDEE couplé à LMDZ

PhD S. Ait Mesbah

Some examples : 1D south Great Plaines

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ORCHIDEE couplé à LMDZ

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Thanks :Rachida El Ouaraini and Bouchra Sadiki,UM6P 2022

2 clear sky days in summer during MOSAI campaign in Lannemezan (Near Pyrénées)

Same physics authorizing less decoupling between The land surface and the atmosphere

1D Case, DEPHY group, A. Maison

2 clear sky days in summer during MOSAI campaign in Lannemezan (Near Pyrénées)

1D Case, DEPHY group, A. Maison

Atmosphere/surface coupling in LMDZOR

,

LMDZ (phylmd)

Planetary boundary layer and surface modules

pbl surface (A_{q} , B_{q} , A_{H} , B_{B} , C_{dh} , A_{u} , B_{u} , A_{v} , B_{v} , C_{dh} , T_{1} , q_{1} , u_{1} , v_{1} , LW_{net} , LW_{down} , Sw_{net}) AcoefH, AcoefQ, BcoefH, BcoefQ cdragh,lwdown,swnet

(is_ter, $ok_veget = n)$ **surf_land_bucket** (soil.F90: soil T, heat capacity, conduction, calcul_flux : sens,flat,tsurf_new Hydro= water budget (snow, precip, Evap)

 $(is_ter, ok_veget = y)$ **surf_land_orchidee**

Call tree

In subroutine PHYSIQ

loop over time steps

....

CALL change srf frac : Update fraction of the sub-surfaces (pctsrf)

CALL pbl_surface Main subroutine for the interface with surface

Calculate net radiation at sub-surface

Loop over the sub-surfaces nsrf

Compress variables (Consider only one surface type and only the points for which the fraction for this sub-surface in not zero)

CALL cdrag: coefficients for turbulent diffusion at surface (cdragh and cdragm)

CALL coef diff turb: coef. turbulent dif. in the atmosphere (ycoefm et ycoefm.)

CALL climb_hq_down downhill for enthalpy H and humidity Q

CALL climb_wind_down downhill for wind (U and V)

CALL surface models for the various surface types: **surf_land, surf_landice, surf_ocean or surf_seaice**.

Each surface model computes:

• evaporation, latent heat flux, sensible heat flux, momentum

• surface temperature, albedo (emissivity), roughness lengths

CALL climb hq up : compute new values of enthalpy H and humidity Q

CALL climb_wind_up : compute new values of wind (U and V)

Uncompress variables : (some variables are per unit of sub-surface fraction, some are per unit of grid surface fraction)

Cumulate in global variables after weighting by sub-surface fractions Surface diagnostics : (T, q, wind are evaluated at a reference level (2m) owing to an interpolation scheme based on the MO laws).

End Loop over the sub-surfaces

Calculate the mean values over all sub-surfaces for some variables **End pbl-surface**

Take home messages

- Atmosphere and surfaces are coupled through turbulent diffusion and radiation
- Different sub-surface are considered (albedo, emissivity, rugosity) for ocean, land, land-ice, sea ice but only one atmosphere is above.
- For each sub-surface one solves a unique diffusion equation from the top of the PBL to the bottom of the soil with an implicit scheme. The surface energy budget allows to find the boundary conditions
- Priority is given to the energy conservation
- The coupling matters : surface forced simulations can produce irrealistic surface fluxes, local surface condition strongly impact near surface variables
- ⚫ Technical note **:** Description of the interface with the surface and the computation of the turbulent diffusion in LMDZ (J.L.Dufresne and J. Ghattas) https://forge.ipsl.jussieu.fr/orchidee/attachment/wiki/Documentation/CouplingLMD Z/Dufresne,%20Ghattas%20-%202009_Coupling-ORC-LMDZ.pdf
- ⚫ Thèse F. Hourdin 1993 (section 3.3.3 and annexes) web page F. Hourdin
- ⚫ Wang F., F. Cheruy, J.L. Dufresne, 2016: The improvement of soil thermodynamics and its effects on land surface meteorology in the IPSL climate model. Geosci. Model Dev., 9, 363-381, 2016 www.geosci-modeldev.net/9/363/2016/
- ⚫ Cheruy et al.,2020 Improved near surface continental climate in IPSL-CM6A-LR by combined evolutions of atmospheric and land surface physics https://agupubs.onlinelibrary.wiley.com/doi/full/10.1029/2019MS002005

Solving the tridiagonal system

$$
\left(\frac{m_l}{\delta t} + K_{l+1} + K_l\right)X_l = \frac{m_l}{\delta t}X_l^0 + K_{l+1}X_{l+1} + K_lX_{l-1}
$$

which may be written as:

At th

At th ,,,,,,,,,,,,,,,,

$$
\left(\delta P_l + R_{l+1}^X + R_l^X\right) X_l = \delta P_l X_l^0 + R_{l+1}^X X_{l+1} + R_l^X X_{l-1} \right) \quad (2 \le l < n)
$$
\nwith $R_l^X = g \delta t K_l$
\ne top (l=n, $\Phi_n = 0$)
\n
$$
\left(\delta P_n + R_n^X\right) X_n = \delta P_n X_n^0 + R_n^X X_{n-1}
$$
\ne bottom:
\n(l=1): $\mathbf{m}_1 \frac{\mathbf{x}_1 - \mathbf{x}_1^0}{\delta t} = \Phi^1_{\mathbf{x}} - \Phi^2_{\mathbf{x}}$
\n
$$
m_1 \frac{X_1 - X_1^0}{\delta t} = K_2(X_2 - X_1) - F_1^X
$$
\n
$$
\left(\delta P_1 + R_1^X\right) X_1 = \delta P_1 X_1^0 + R_2^X X_2 - g \delta t \frac{F_1^X}{F_1}
$$

With F_1^X : flux of *X* at the bottom of the first layer (i.e. between the surface and the atmosphere), positive downward.

$$
K_l = \frac{k_z \rho^2 g}{P_{l-1} - P_l}
$$

 α

Solving the tridiagonal system

Starting from top:

$$
(\delta P_n + R_n^X) X_n = \delta P_n X_n^0 + R_n^X X_{n-1}
$$

can be written as:

$$
X_n = C_n^X + D_n^X X_{n-1}
$$

with

$$
C_n^X = \frac{X_n^0 \delta P_n}{\delta P_n + R_n^X}
$$

$$
D_n^X = \frac{R_n^X}{\delta P_n + R_n^X}
$$

with $R_l^X = g \delta t K_l$

$$
\left(\delta P_l + R_{l+1}^X \left(1 - D_{l+1}^X\right) + R_l^X\right) X_l = \delta P_l X_l^0 + R_{l+1}^X C_{l+1}^X + R_l^X X_{l-1}
$$

with $R_l^X = g \delta t K_l$

So we obtain by recourrence:

$$
X_l = C_l^X + D_l^X X_{l-1} \qquad (2 \le l \le n)
$$

with, for $(2 \leq l < n)$

$$
C_l^X = \frac{X_l^0 \delta P_l + R_{l+1}^X C_{l+1}^X}{\delta P_l + R_l^X + R_{l+1}^X (1 - D_{l+1}^X)}
$$

$$
D_l^X = \frac{R_l^X}{\delta P_l + R_l^X + R_{l+1}^X (1 - D_{l+1}^X)}
$$

In LMDZ routine calc_coef

depend only on properties in the layers above and the variables at the previous time step.

$$
\Phi_{x}^{1-1/2} = -K_{1-1/2} (X_{1} - X_{1-1})
$$

 $t + \delta t$

.

t

k

k